## FEATURES

Automatically Senses Sample Frequencies
No Programming Required
Attenuates Sample Clock Jitter
3.3 V to 5 V Input and 3.3 V Core Supply Voltages

Accepts 16-/18-/20-/24-Bit Data
Up to 192 kHz Sample Rate
Input/Output Sample Ratios from 7.75:1 to 1:8
Bypass Mode
Multiple AD1895 TDM Daisy-Chain Mode
128 dB Signal-to-Noise and Dynamic Range
(A-Weighted, 20 Hz to 20 kHz BW)
Up to -122 dB THD + N
Linear Phase FIR Filter
Hardware Controllable Soft Mute
Supports $256 \times \mathrm{f}_{\mathrm{S}}, 512 \times \mathrm{f}_{\mathrm{S}}$, or $768 \times \mathrm{f}_{\mathrm{S}}$ Master Mode Clock
Flexible 3-Wire Serial Data Port with Left-Justified, $I^{2}$ S, Right-Justified (16-, 18-, 20-, 24-Bit), and TDM Serial Port Modes
Master/Slave Input and Output Modes
28-Lead SSOP Plastic Package

## APPLICATIONS

Home Theater Systems, Automotive Audio Systems, DVD, DVD-R, CD-R, Set-Top Boxes, Digital Audio Effects Processors

## PRODUCT OVERVIEW

The AD1895 is a 24 -bit, high performance, single-chip, second generation asynchronous sample rate converter. Based upon Analog Devices' experience with its first asynchronous sample rate converter, the AD1890, the AD1895 offers improved performance and additional features. This improved performance includes a THD +N range of -115 dB to -122 dB depending on sample rate and input frequency, 128 dB (A-Weighted) dynamic range, 192 kHz sampling frequencies for both input and output sample rates, improved jitter rejection, and 1:8 upsampling and 7.75:1 downsampling ratios. Additional features include more serial formats, a bypass mode, and better interfacing to digital signal processors.

The AD1895 has a 3-wire interface for the serial input and output ports that supports left-justified, $\mathrm{I}^{2} \mathrm{~S}$, and right-justified (16-, 18-, 20-, 24-bit) modes. Additionally, the serial output port supports TDM Mode for daisy-chaining multiple AD1895s to

a digital signal processor. The serial output data is dithered down to 20,18 , or 16 bits when 20 -, 18 -, or 16 -bit output data is selected. The AD1895 sample rate converts the data from the serial input port to the sample rate of the serial output port. The sample rate at the serial input port can be asynchronous with respect to the output sample rate of the output serial port. The master clock to the AD1895, MCLK, can be asynchronous to both the serial input and output ports.
MCLK can either be generated off-chip or on-chip by the AD1895 master clock oscillator. Since MCLK can be asynchronous to the input or output serial ports, a crystal can be used to generate MCLK internally to reduce noise and EMI emissions on the board. When MCLK is synchronous to either the output or input serial port, the AD1895 can be configured in a master mode where MCLK is divided down and used to generate the left/right and bit clocks for the serial port that is synchronous to MCLK. The AD1895 supports master modes of $256 \times \mathrm{f}_{\mathrm{S}}, 512 \times \mathrm{f}_{\mathrm{S}}$, and $768 \times \mathrm{f}_{\mathrm{S}}$ for both input and output serial ports.

Conceptually, the AD1895 interpolates the serial input data by a rate of $2^{20}$ and samples the interpolated data stream by the output sample rate. In practice, a 64 -tap FIR filter with $2^{20}$ polyphases, a FIFO, a digital servo loop that measures the time difference between input and output samples within 5 ps , and a digital circuit to track the sample rate ratio are used to perform the interpolation and output sampling. Refer to the Theory of Operation section. The digital servo loop and sample rate ratio circuit automatically track the input and output sample rates.
(continued on page 15)

[^0]REV. B

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TEST CONDITIONS, UNLESS OTHERWISE NOTED.

| Supply Voltages |  |
| :---: | :---: |
| VDD_CORE | 3.3 V |
| VDD_IO | 5.0 V or 3.3 V |
| Ambient Temperature | $25^{\circ} \mathrm{C}$ |
| Input Clock | 30.0 MHz |
| Input Signal | $1.000 \mathrm{kHz}, 0 \mathrm{dBFS}$ |
| Measurement Bandwidth | 20 to $\mathrm{f}_{\text {S_OUT }} / 2 \mathrm{~Hz}$ |
| Word Width | 24 Bits |
| Load Capacitance | . 50 pF |
| Input Voltage High | 2.4 V |
| Input Voltage Low | 0.8 V |

DIGITAL PERFORMANCE (VDD_CORE $=3.3 \mathrm{~V} \pm 5 \%, V D D \_I O=5.0 \mathrm{~V} \pm 10 \%$ )

| Parameter | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: |
| RESOLUTION | 24 |  |  | Bits |
| SAMPLE RATE @ MCLK_IN = 30 MHz | 6 |  | 215 | kHz |
| SAMPLE RATE (@) OTHER MASTER CLOCKS) ${ }^{1}$ | MCLK_IN/5000 $\leq \mathrm{f}_{\text {S_MAX }}<$ MCLK_IN/138 |  |  | kHz |
| SAMPLE RATE RATIOS <br> Upsampling <br> Downsampling | $\begin{aligned} & 1: 8 \\ & 7.75: 1 \end{aligned}$ |  |  |  |
| ```DYNAMIC RANGE \({ }^{2}\) ( 20 Hz to \(\mathrm{f}_{\text {S_out }} / 2,1 \mathrm{kHz},-60 \mathrm{dBFS}\) Input) A-Weighted \(44.1 \mathrm{kHz}: 48 \mathrm{kHz}\) \(48 \mathrm{kHz}: 44.1 \mathrm{kHz}\) \(48 \mathrm{kHz}: 96 \mathrm{kHz}\) \(44.1 \mathrm{kHz}: 192 \mathrm{kHz}\) \(96 \mathrm{kHz}: 48 \mathrm{kHz}\) \(192 \mathrm{kHz}: 32 \mathrm{kHz}\) ( 20 Hz to \(\mathrm{f}_{\text {S_out }} / 2,1 \mathrm{kHz},-60 \mathrm{dBFS}\) Input) No Filter \(44.1 \mathrm{kHz}: 48 \mathrm{kHz}\) \(48 \mathrm{kHz}: 44.1 \mathrm{kHz}\) \(48 \mathrm{kHz}: 96 \mathrm{kHz}\) \(44.1 \mathrm{kHz}: 192 \mathrm{kHz}\) 96 kHz: 48 kHz \(192 \mathrm{kHz}: 32 \mathrm{kHz}\)``` |  | $\begin{aligned} & 128 \\ & 128 \\ & 128 \\ & 128 \\ & 127 \\ & 127 \\ & 125 \\ & 125 \\ & 125 \\ & 125 \\ & 124 \\ & 124 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB |
| TOTAL HARMONIC DISTORTION + NOISE ${ }^{2}$ <br> ( 20 Hz to $\mathrm{f}_{\text {S_out }} / 2,1 \mathrm{kHz}, 0 \mathrm{dBFS}$ Input) No Filter Worst-Case ( $48 \mathrm{kHz}: 96 \mathrm{kHz})^{3}$ <br> $44.1 \mathrm{kHz}: 48 \mathrm{kHz}$ <br> $48 \mathrm{kHz}: 44.1 \mathrm{kHz}$ <br> $48 \mathrm{kHz}: 96 \mathrm{kHz}$ <br> $44.1 \mathrm{kHz}: 192 \mathrm{kHz}$ <br> $96 \mathrm{kHz}: 48 \mathrm{kHz}$ <br> $192 \mathrm{kHz}: 32 \mathrm{kHz}$ | -115 | $\begin{aligned} & -120 \\ & -119 \\ & -118 \\ & -120 \\ & -122 \\ & -122 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB |
| INTERCHANNEL GAIN MISMATCH |  | 0.0 |  | dB |
| INTERCHANNEL PHASE DEVIATION |  | 0.0 |  | Degrees |
| MUTE ATTENUATION (24 BITS WORD WIDTH)(A- | EIGHT) | -127 |  | dB |

[^1]DIGITAL TIMING $\left(-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+105^{\circ} \mathrm{C}\right.$, VDD_CORE $\left.=3.3 \mathrm{~V} \pm 5 \%, \mathrm{VDD} \_I O=5.0 \mathrm{~V} \pm 10 \%\right)$

| Parameter ${ }^{1}$ |  | Min | Max | Unit |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\text {MCLKI }}$ | MCLK_IN Period | 33.3 |  | ns |
| $\mathrm{f}_{\text {MCLK }}$ | MCLK_IN Frequency |  | $30.0^{2,3}$ | MHz |
| $\mathrm{t}_{\text {MPWH }}$ | MCLK_IN Pulsewidth High | 9 |  | ns |
| $\mathrm{t}_{\text {MPWL }}$ | MCLK_IN Pulsewidth Low | 12 |  | ns |
| INPUT SERIAL PORT TIMING |  |  |  |  |
| $\mathrm{t}_{\text {LRIS }}$ | LRCLK_I Setup to SCLK_I | 8 |  | ns |
| $\mathrm{t}_{\text {SIH }}$ | SCLK_I Pulsewidth High | 8 |  | ns |
| $\mathrm{t}_{\text {SIL }}$ | SCLK_I Pulsewidth Low | 8 |  | ns |
| $\mathrm{t}_{\text {DIS }}$ | SDATA_I Setup to SCLK_I Rising Edge | 8 |  | ns |
| $\mathrm{t}_{\text {DIH }}$ | SDATA_I Hold from SCLK_I Rising Edge | 3 |  | ns |
| OUTPUT SERIAL PORT TIMING |  |  |  |  |
| $\mathrm{t}_{\text {TDMS }}$ | TDM_IN Setup to SCLK_O Falling Edge | 3 |  | ns |
| $\mathrm{t}_{\text {TDMH }}$ | TDM_IN Hold from SCLK_O Falling Edge | 3 |  | ns |
| $\mathrm{t}_{\text {DOPD }}$ | SDATA_O Propagation Delay from SCLK_O, LRCLK_O |  | 20 | ns |
| $\mathrm{t}_{\text {DOH }}$ | SDATA_O Hold from SCLK_O | 3 |  | ns |
| $\mathrm{t}_{\text {LROS }}$ | LRCLK_O Setup to SCLK_O (TDM Mode Only) | 5 |  | ns |
| $\mathrm{t}_{\text {LROH }}$ | LRCLK_O Hold from SCLK_O (TDM Mode Only) | 3 |  | ns |
| $\mathrm{t}_{\text {SOH }}$ | SCLK_O Pulsewidth High | 10 |  | ns |
| $\mathrm{t}_{\text {SOL }}$ | SCLK_O Pulsewidth Low | 5 |  | ns |
| $\mathrm{t}_{\text {RSTL }}$ | RESET Pulsewidth Low | 200 |  | ns |

## NOTES

${ }^{1}$ Refer to Timing Diagrams section.
${ }^{2}$ The maximum possible sample rate is: $\mathrm{FS}_{\text {MAX }}=\mathrm{f}_{\text {MCLK }} / 138$.
${ }^{3} \mathrm{f}_{\text {MCLK }}$ of up to 34 MHz is possible under the following conditions: $0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C}, 45 / 55$ or better MCLK_IN duty cycle.
Specifications subject to change without notice.

## TIMING DIAGRAMS



MCLK_IN


RESET


Figure 2. $\overline{R E S E T}$ Timing


Figure 3. MCLK_IN Timing

## AD1895-SPECIFICATIONS

DIGITAL FILTERS (VDD_CORE = $3.3 \mathrm{~V} \pm 5 \%$, VDD_IO = 5.0 $\mathrm{V} \pm 10 \%$ )

| Parameter | Min | Typ | Max | Unit |
| :--- | :--- | :--- | :--- | :--- |
| Pass Band |  |  | $0.4535 \mathrm{f}_{\text {S_out }}$ | Hz |
| Pass-Band Ripple |  | $\pm 0.016$ | dB |  |
| Transition Band | $0.4535 \mathrm{f}_{\text {S_out }}$ | $0.5465 \mathrm{f}_{\text {S_out }}$ | Hz |  |
| Stop Band | $0.5465 \mathrm{f}_{\text {S_out }}$ | -125 | Hz |  |
| Stop-Band Attenuation | Refer to the Group Delay Equations Section |  | dB |  |
| Group Delay |  |  |  |  |

Specifications subject to change without notice.

DIGITAL I/O CHARACTERISTICS (VDD_CORE $=3.3 \mathrm{~V} \pm 5 \%$, VDD_IO $=5.0 \mathrm{~V} \pm 10 \%$ )

| Parameter | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: |
| Input Voltage High ( $\mathrm{V}_{\mathrm{IH}}$ ) | 2.4 |  |  | V |
| Input Voltage Low ( $\mathrm{V}_{\mathrm{IL}}$ ) |  |  | 0.8 | V |
| Input Leakage ( $\mathrm{I}_{\mathrm{IH}} @ \mathrm{~V}_{\mathrm{IH}}=5 \mathrm{~V}$ ) |  |  | +2 | $\mu \mathrm{A}$ |
| Input Leakage ( $\mathrm{I}_{\mathrm{IL}}$ @ $\mathrm{V}_{\text {IL }}=0 \mathrm{~V}$ ) |  |  | -2 | $\mu \mathrm{A}$ |
| Input Capacitance |  | 5 | 10 | pF |
| Output Voltage High ( $\left.\mathrm{V}_{\mathrm{OH}} @ \mathrm{I}_{\mathrm{OH}}=-4 \mathrm{~mA}\right)$ | VDD_CORE - 0.5 | VDD_CORE - 0.4 |  | V |
| Output Voltage Low ( $\mathrm{V}_{\mathrm{OL}}$ @ $\left.\mathrm{I}_{\mathrm{OL}}=+4 \mathrm{~mA}\right)$ |  | 0.2 | 0.5 | V |
| Output Source Current High ( $\mathrm{I}_{\mathrm{OH}}$ ) |  |  | -4 | mA |
| Output Sink Current Low ( $\mathrm{I}_{\mathrm{OL}}$ ) |  |  | +4 | mA |

Specifications subject to change without notice.

## POWER SUPPLIES

| Parameter | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: |
| SUPPLY VOLTAGE <br> VDD_CORE <br> VDD_IO* | $\begin{aligned} & 3.135 \\ & \text { VDD_CORE } \end{aligned}$ | $\begin{aligned} & 3.3 \\ & 3.3 / 5.0 \end{aligned}$ | $\begin{aligned} & 3.465 \\ & 5.5 \end{aligned}$ | $\begin{aligned} & \text { V } \\ & \text { V } \end{aligned}$ |
| ACTIVE SUPPLY CURRENT <br> I_CORE_ACTIVE <br> $48 \mathrm{kHz}: 48 \mathrm{kHz}$ <br> 96 kHz: 96 kHz <br> $192 \mathrm{kHz}: 192 \mathrm{kHz}$ <br> I_IO_ACTIVE |  | $\begin{aligned} & 20 \\ & 26 \\ & 43 \\ & 2 \end{aligned}$ |  | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \end{aligned}$ |
| POWER-DOWN SUPPLY CURRENT: (ALL CLOCKS <br> I_CORE_PWRDN <br> I_IO_PWRDN | TOPPED) | $\begin{aligned} & 0.5 \\ & 10 \end{aligned}$ |  | $\begin{aligned} & \mathrm{mA} \\ & \mu \mathrm{~A} \end{aligned}$ |

*For 3.3 V tolerant inputs, VDD_IO supply should be set to 3.3 V ; however, VDD_CORE supply voltage should not exceed VDD_IO.
Specifications subject to change without notice.

POWER SUPPLIES (VDD_CORE $=3.3 \mathrm{~V} \pm 5 \%$, VDD_IO $=5.0 \mathrm{~V} \pm 10 \%$ )

| Parameter | Min | Typ | Max |
| :--- | :--- | :--- | :---: |
| TOTAL ACTIVE POWER DISSIPATION |  |  | Unit |
| $48 \mathrm{kHz}: 48 \mathrm{kHz}$ | 65 | mW |  |
| $96 \mathrm{kHz}: 96 \mathrm{kHz}$ |  | 85 | mW |
| $192 \mathrm{kHz}: 192 \mathrm{kHz}$ | 132 | mW |  |
| TOTAL POWER-DOWN DISSIPATION (RESET LOW) | 2 | mW |  |

Specifications subject to change without notice.

TEMPERATURE RANGE

| Parameter | Min | Typ | Max | Unit |
| :--- | :--- | :--- | :--- | :--- |
| Specifications Guaranteed |  | 25 |  | ${ }^{\circ} \mathrm{C}$ |
| Functionality Guaranteed | -40 |  | +105 | ${ }^{\circ} \mathrm{C}$ |
| Storage | -55 | 109 | ${ }^{\circ} \mathrm{C}$ |  |
| Thermal Resistance, $\theta_{\text {JA }}$ (Junction to Ambient) |  | 100 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |  |

Specifications subject to change without notice.

## ABSOLUTE MAXIMUM RATINGS*


*Stresses greater than those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| AD1895AYRS | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 28 -Lead SSOP | RS-28 |
| AD1895AYRSRL | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 28 -Lead SSOP | RS-28 on 13" Reel |

## CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD1895 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

PIN FUNCTION DESCRIPTIONS

| Pin No. | IN/OUT (I/O) | Mnemonic | Description |
| :--- | :--- | :--- | :--- |
| 1 | IN | NC | No Connect |
| 2 | IN | MCLK_IN | Master Clock or Crystal Input |
| 3 | OUT | MCLK_OUT | Master Clock Output or Crystal Output |
| 4 | IN | SDATA_I | Input Serial Data (at Input Sample Rate) |
| 5 | IN/OUT | SCLK_I | Master/Slave Input Serial Bit Clock |
| 6 | IN/OUT | LRCLK_I | Master/Slave Input Left/Right Clock |
| 7 | IN | VDD_IO | 3.3 V/5 V Input/Output Digital Supply Pin |
| 8 | IN | DGND | Digital Ground Pin |
| 9 | IN | BYPASS | ASRC Bypass Mode, Active High |
| 10 | IN | SMODE_IN_0 | Input Port Serial Interface Mode Select Pin 0 |
| 11 | IN | SMODE_IN_1 | Input Port Serial Interface Mode Select Pin 1 |
| 12 | IN | SMODE_IN_2 | Input Port Serial Interface Mode Select Pin 2 |
| 13 | IN | RESET | Reset Pin, Active Low |
| 14 | IN | MUTE_IN | Mute Input Pin—Active High Normally Connected to MUTE_OUT |
| 15 | OUT | MUTE_OUT | Output Mute Control-Active High |
| 16 | IN | WLNGTH_OUT_1 | Hardware Selectable Output Wordlength-Select Pin 1 |
| 17 | IN | WLNGTH_OUT_0 | Hardware Selectable Output Wordlength—Select Pin 0 |
| 18 | IN | SMODE_OUT_1 | Output Port Serial Interface Mode Select Pin 1 |
| 19 | IN | SMODE_OUT_0 | Output Port Serial Interface Mode Select Pin 0 |
| 20 | IN | TDM_IN | Serial Data Input* (Only for Daisy-Chain Mode). Ground when not used. |
| 21 | IN | DGND | Digital Ground Pin |
| 22 | IN | VDD_CORE | 3.3 V Digital Supply Pin |
| 23 | OUT | SDATA_O | Output Serial Data (at Output Sample Rate) |
| 24 | IN/OUT | LRCLK_O | Master/Slave Output Left/Right Clock |
| 25 | IN/OUT | SCLK_O | Master/Slave Output Serial Bit Clock |
| 26 | IN | MMODE_0 | Master/Slave Clock Ratio Mode Select Pin 0 |
| 27 | IN | MMODE_1 | Master/Slave Clock Ratio Mode Select Pin 1 |
| 28 | IN | MMODE_2 | Master/Slave Clock Ratio Mode Select Pin 2 |

*Also used to input matched-phase mode data.

## PIN CONFIGURATION



## Typical Performance Characteristics-AD1895



TPC 1. Wideband FFT Plot (16 k Points) 0 dBFS 1 kHz Tone, 48 kHz: 48 kHz (Asynchronous)


TPC 2. Wideband FFT Plot (16 k Points) 0 dBFS 1 kHz Tone, 44.1 kHz: 48 kHz (Asynchronous)


TPC 3. Wideband FFT Plot (16 k Points) 48 kHz: 96 kHz, 0 dBFS 1 kHz Tone


TPC 4. Wideband FFT Plot (16 k Points) 44.1 kHz: 192 kHz, 0 dBFS 1 kHz Tone


TPC 5. Wideband FFT Plot (16 k Points) 48 kHz: 44.1 kHz, 0 dBFS 1 kHz Tone


TPC 6. Wideband FFT Plot (16 k Points) 96 kHz: 48 kHz, 0 dBFS 1 kHz Tone


TPC 7. Wideband FFT Plot (16 k Points) 192 kHz: 48 kHz, 0 dBFS 1 kHz Tone


TPC 8. Wideband FFT Plot (16 k Points) 48 kHz: 48 kHz -60 dBFS 1 kHz Tone (Asynchronous)


TPC 9. Wideband FFT Plot (16 k Points) 44.1 kHz: 48 kHz, -60 dBFS 1 kHz Tone


TPC 10. Wideband FFT Plot (16 k Points) 48 kHz: 96 kHz, -60 dBFS 1 kHz Tone


TPC 11. Wideband FFT Plot (16 k Points) 44.1 kHz: 192 kHz, -60 dBFS 1 kHz Tone


TPC 12. Wideband FFT Plot (16 k Points) 48 kHz: 44.1 kHz, -60 dBFS 1 kHz Tone


TPC 13. Wideband FFT Plot (16 k Points) 96 kHz: 48 kHz, -60 dBFS 1 kHz Tone


TPC 14. Wideband FFT Plot (16 k Points) 192 kHz: 48 kHz, -60 dBFS 1 kHz Tone


TPC 15. IMD, 10 kHz and $11 \mathrm{kHz}, 0 \mathrm{dBFS}$ Tone, 44:1 kHz: 48 kHz


TPC 16. IMD, 10 kHz and $11 \mathrm{kHz}, 0 \mathrm{dBFS}$ Tone, 96 kHz: 48 kHz


TPC 17. IMD, 10 kHz and $11 \mathrm{kHz}, 0 \mathrm{dBFS}$ Tone, 48 kHz: 44.1 kHz


TPC 18. Wideband FFT Plot (16 k Points) 44.1 kHz: 48 kHz, 0 dBFS 20 kHz Tone


TPC 19. Wideband FFT Plot (16 k Points) 192 kHz: 192 kHz, 0 dBFS 80 kHz Tone


TPC 20. Wideband FFT Plot (16 k Points) 48 kHz: 48 kHz, 0 dBFS 20 kHz Tone


TPC 21. Wideband FFT Plot (16 k Points) 48 kHz: 44:1 kHz, 0 dBFS 20 kHz Tone


TPC 22. Wideband FFT Plot (16 k Points) 48 kHz: 96 kHz, 0 dBFS 20 kHz Tone


TPC 23. Wideband FFT Plot (16 k Points) 96 kHz: 48 kHz, 0 dBFS 20 kHz Tone


TPC 24. THD + N vs. Output Sample Rate, $f_{S_{-} N}=192 \mathrm{kHz}$, 0 dBFS 1 kHz Tone


TPC 25. THD $+N$ vs. Output Sample Rate, $f_{S_{-} I N}=48 \mathrm{kHz}$, 0 dBFS 1 kHz Tone


TPC 26. $T H D+N$ vs. Output Sample Rate, $f_{S_{-} I N}=$ $44.1 \mathrm{kHz}, 0 \mathrm{dBFS} 1 \mathrm{kHz}$ Tone


TPC 27. THD $+N$ vs. Output Sample Rate, $f_{S_{-} I N}=32 \mathrm{kHz}$, 0 dBFS 1 kHz Tone


TPC 28. THD $+N$ vs. Output Sample Rate, $f_{S_{-} I N}=96 \mathrm{kHz}$, 0 dBFS 1 kHz Tone


TPC 29. DNR (Unweighted) vs. Output Sample Rate, $f_{S_{-} I N}=192 \mathrm{kHz},-60 \mathrm{dBFS} 1 \mathrm{kHz}$ Tone


TPC 30. DNR (Unweighted) vs. Output Sample Rate, $f_{S_{-} / \mathrm{N}}=32 \mathrm{kHz},-60 \mathrm{dBFS} 1 \mathrm{kHz}$ Tone


TPC 31. DNR (Unweighted) vs. Output Sample Rate, $f_{S_{-} I N}=96 \mathrm{kHz},-60 \mathrm{dBFS} 1 \mathrm{kHz}$ Tone


TPC 32. Digital Filter Frequency Response


TPC 33. DNR (Unweighted) vs. Output Sample Rate, $f_{S_{-} I N}=48 \mathrm{kHz},-60 \mathrm{dBFS} 1 \mathrm{kHz}$ Tone


TPC 34. DNR (Unweighted) vs. Output Sample Rate, $f_{S_{-} I N}=44.1 \mathrm{kHz},-60 \mathrm{dBFS} 1 \mathrm{kHz}$ Tone


TPC 35. Pass-Band Ripple, 192 kHz: 48 kHz


TPC 36. Linearity Error, $48 \mathrm{kHz}: 48 \mathrm{kHz}, 0 \mathrm{dBFS}$ to -140 dBFS Input, 200 Hz Tone


TPC 37. Linearity Error, $48 \mathrm{kHz}: 44.1 \mathrm{kHz}, 0 \mathrm{dBFS}$ to -140 dBFS Input, 200 Hz Tone


TPC 38. Linearity Error, 96 kHz: 48 kHz, 0 dBFS to -140 dBFS Input, 200 Hz Tone


TPC 39. Linearity Error, $44.1 \mathrm{kHz}: 48 \mathrm{kHz}, 0 \mathrm{dBFS}$ to -140 dBFS Input, 200 Hz Tone


TPC 40. Linearity Error, $48 \mathrm{kHz}: 96 \mathrm{kHz}, 0 \mathrm{dBFS}$ to -140 dBFS Input, 200 Hz Tone


TPC 41. Linearity Error, $44.1 \mathrm{kHz}: 192 \mathrm{kHz}, 0 \mathrm{dBFS}$ to -140 dBFS Input, 200 Hz Tone


TPC 42. Linearity Error, 192 kHz: $44.1 \mathrm{kHz}, 0 \mathrm{dBFS}$ to -140 dBFS Input, 200 Hz Tone


TPC 43. THD + N vs. Input Amplitude, 48 kHz: 44.1 kHz, 1 kHz Tone


TPC 44. THD + N vs. Input Amplitude, 96 kHz: 48 kHz, 1 kHz Tone


TPC 45. THD + N vs. Input Amplitude, 44.1 kHz: 48 kHz, 1 kHz Tone


TPC 46. THD + N vs. Input Amplitude, 48 kHz: 96 kHz, 1 kHz Tone


TPC 47. THD + N vs. Input Amplitude, 44.1 kHz: 192 kHz, 1 kHz Tone


TPC 48. THD + N vs. Input Amplitude, 192 kHz: 48 kHz, 1 kHz Tone


TPC 49. THD + N vs. Frequency Input, 48 kHz: 44.1 kHz, 0 dBFS


TPC 50. THD + N vs. Frequency Input, 44.1 kHz: 48 kHz, 0 dBFS


TPC 51. THD + N vs. Frequency Input, 48 kHz: 96 kHz, 0 dBFS


TPC 52. THD + N vs. Frequency Input, 96 kHz: 48 kHz, 0 dBFS

PRODUCT OVERVIEW (continued from page 1)
The digital servo loop measures the time difference between input and output sample rates within 5 ps . This is necessary in order to select the correct polyphase filter coefficient. The digital servo loop has excellent jitter rejection for both input and output sample rates as well as the master clock. The jitter rejection begins at less than 1 Hz . This requires a long settling time whenever $\overline{\text { RESET }}$ is deasserted or when the input or output sample rate changes. To reduce the settling time, upon deassertion of $\overline{\text { RESET }}$ or a change in a sample rate, the digital servo loop enters the Fast Settling Mode. When the digital servo loop has adequately settled in the Fast Mode, it switches into the Normal or Slow Settling Mode and continues to settle until the time difference measurement between input and output sample rates is within 5 ps . During

Fast Mode, the MUTE_OUT signal is asserted high. Normally, the MUTE_OUT is connected to the MUTE_IN pin. The MUTE_IN signal is used to softly mute the AD1895 upon assertion and softly unmute the AD1895 when it is deasserted. The sample rate converter of the AD1895 can be bypassed altogether using the Bypass Mode. In Bypass Mode, the AD1895's serial input data is directly passed to the serial output port without any dithering. This is useful for passing through nonaudio data or when the input and output sample rates are synchronous to one another and the sample rate ratio is exactly 1 to 1 .
The AD1895 is a $3.3 \mathrm{~V}, 5 \mathrm{~V}$ input tolerant part and is available in a 28 -lead SSOP SMD package. The AD1895 is 5 V input tolerant only when the VDD_IO supply pin is supplied with 5 V .

## AD1895

## ASRC FUNCTIONAL OVERVIEW THEORY OF OPERATION

Asynchronous sample rate conversion is converting data from one clock source at some sample rate to another clock source at the same or different sample rate. The simplest approach to asynchronous sample rate conversion is the use of a zero-order hold between two samplers as shown in Figure 4. In an asynchronous system, T 2 is never equal to T 1 nor is the ratio between T 2 and T 1 rational. As a result, samples at $\mathrm{f}_{\mathrm{S} \text { _out }}$ will be repeated or dropped, producing an error in the resampling process. The frequency domain shows the wide side lobes that result from this error when the sampling of $\mathrm{f}_{\text {S_out }}$ is convolved with the attenuated images from the $\sin (\mathrm{x}) / \mathrm{x}$ nature of the zero-order hold. The images at $f_{\text {S_IN }}$, dc signal images, of the zero-order hold are infinitely attenuated. Since the ratio of T 2 to T 1 is an irrational number, the error resulting from the resampling at $\mathrm{f}_{\text {S_out }}$ can never be eliminated. However, the error can be significantly reduced through interpolation of the input data at $\mathrm{f}_{\mathrm{S}_{\text {_ }}}$. The AD1895 is conceptually interpolated by a factor of $2^{20}$.


Figure 4. Zero-Order Hold Being Used by $f_{S_{-} \text {out }}$ to Resample Data from $f_{S_{-} I N}$

THE CONCEPTUAL HIGH INTERPOLATION MODEL Interpolation of the input data by a factor of $2^{20}$ involves placing $\left(2^{20}-1\right)$ samples between each $\mathrm{f}_{\text {S_IN }}$ sample. Figure 5 shows both the time domain and the frequency domain of interpolation by a factor of $2^{20}$. Conceptually, interpolation by $2^{20}$ would
involve the steps of zero-stuffing $\left(2^{20}-1\right)$ a number of samples between each $\mathrm{f}_{\text {S_IN }^{\prime}}$ sample and convolving this interpolated signal with a digital low-pass filter to suppress the images. In the time domain, it can be seen that $\mathrm{f}_{\mathrm{S}_{\text {_out }}}$ selects the closest $\mathrm{f}_{\mathrm{S}_{-} \mathrm{IN}} \times 2^{20}$ sample from the zero-order hold as opposed to the nearest $\mathrm{f}_{\mathrm{S}_{\text {_I }}}$ sample in the case of no interpolation. This significantly reduces the resampling error.


Figure 5. Time Domain of the Interpolation and Resampling
In the frequency domain shown in Figure 6, the interpolation expands the frequency axis of the zero-order hold. The images from the interpolation can be sufficiently attenuated by a good low-pass filter. The images from the zero-order hold are now pushed by a factor of $2^{20}$ closer to the infinite attenuation point of the zero-order hold, which is $\mathrm{f}_{\mathrm{S}_{-} \mathrm{IN}} \times 2^{20}$. The images at the zero-order hold are the determining factor for the fidelity of the output at $\mathrm{f}_{\text {S_out. }}$. The worst-case images can be computed from the zero-order hold frequency response, maximum image $=$ $\sin \left(\pi \times F / f_{S_{-} I N T E R P}\right) /\left(\pi \times F / f_{\left.S_{\text {INTERP }}\right)}\right) . F$ is the frequency of the worst-case image, which would be $2^{20} \times f_{S_{-} I N} \pm f_{S_{-} I N} / 2$, and $f_{S_{-} I N T E R P}$ is $f_{S_{-} I N} \times 2^{20}$.
The following worst-case images would appear for $f_{S_{-} I N}=$ 192 kHz:

Image at $f_{S_{-I N T E R P}}-96 \mathrm{kHz}=-125.1 \mathrm{~dB}$
Image at $f_{S_{-} I N T E R P}+96 \mathrm{kHz}=-125.1 \mathrm{~dB}$


Figure 6. Frequency Domain of the Interpolation and Resampling

## HARDWARE MODEL

The output rate of the low-pass filter of Figure 5 would be the interpolation rate, $2^{20} \times 192000 \mathrm{kHz}=201.3 \mathrm{GHz}$. Sampling at a rate of 201.3 GHz is clearly impractical, not to mention the number of taps required to calculate each interpolated sample. However, since interpolation by $2^{20}$ involves zero-stuffing $2^{20}-1$ samples between each $\mathrm{f}_{\mathrm{S}_{\text {I }}}$ sample, most of the multiplies in the low-pass FIR filter are by zero. A further reduction can be realized by the fact that since only one interpolated sample is taken at the output at the $\mathrm{f}_{\text {s_out }}$ rate, only one convolution needs to be performed per $\mathrm{f}_{\mathrm{S}_{\text {_ out }}}$ period instead of $2^{20}$ convolutions. A 64-tap FIR filter for each $\mathrm{f}_{\text {S_out }}$ sample is sufficient to suppress the images caused by the interpolation.
The difficulty with the above approach is that the correct interpolated sample needs to be selected upon the arrival of $\mathrm{f}_{\text {S_OUT }}$. Since there are $2^{20}$ possible convolutions per $\mathrm{f}_{\mathrm{S} \text { _out }}$ period, the arrival of the $\mathrm{f}_{\text {S_OUT }}$ clock must be measured with an accuracy of $1 / 201.3 \mathrm{GHz}=4.96 \mathrm{ps}$. Measuring the $\mathrm{f}_{\text {S_OUT }}$ period with a clock of 201.3 GHz frequency is clearly impossible; instead, several coarse measurements of the $\mathrm{f}_{\text {S_out }}$ clock period are made and averaged over time.
Another difficulty with the above approach is the number of coefficients required. Since there are $2^{20}$ possible convolutions with a 64 -tap FIR filter, there needs to be $2^{20}$ polyphase coefficients for each tap, which requires a total of $2^{26}$ coefficients. To reduce the number of coefficients in ROM, the AD1895 stores a small subset of coefficients and performs a high order interpolation between the stored coefficients. So far, the above approach works for the case of $f_{S_{\text {_OUT }}}>f_{\text {S_IN }^{\prime}}$. However, in the case when the output sample rate, $\mathrm{f}_{\mathrm{S} \text { _out }}$, is less than the input sample
rate, $\mathrm{f}_{\mathrm{S}_{\mathrm{B}} \mathrm{IN}}$, the ROM starting address, input data, and length of the convolution must be scaled. As the input sample rate rises over the output sample rate, the antialiasing filter's cutoff frequency has to be lowered because the Nyquist frequency of the output samples is less than the Nyquist frequency of the input samples. To move the cutoff frequency of the antialiasing filter, the coefficients are dynamically altered and the length of the convolution is increased by a factor of $\mathrm{f}_{\mathrm{S}_{-}} / \mathrm{f}_{\mathrm{S}_{-} \text {out }}$. This technique is supported by the Fourier transform property that if $f(t)$ is $F(\omega)$, then $f(k \times t)$ is $F(\omega / k)$. Thus, the range of decimation is simply limited by the size of the RAM.

## THE SAMPLE RATE CONVERTER ARCHITECTURE

The architecture of the sample rate converter is shown in Figure 7. The sample rate converter's FIFO block adjusts the left and right input samples and stores them for the FIR filter's convolution cycle. The $\mathrm{f}_{\mathrm{S}_{\mathrm{I}} \mathrm{IN}}$ counter provides the write address to the FIFO block and the ramp input to the digital servo loop. The ROM stores the coefficients for the FIR filter convolution and performs a high order interpolation between the stored coefficients. The sample rate ratio block measures the sample rate for dynamically altering the ROM coefficients and scaling of the FIR filter length as well as the input data. The digital servo loop automatically tracks the $\mathrm{f}_{\text {S_IN }}$ and $\mathrm{f}_{\text {S_OUT }}$ sample rates and provides the RAM and ROM start addresses for the start of the FIR filter convolution.


Figure 7. Architecture of the Sample Rate Converter
The FIFO receives the left and right input data and adjusts the amplitude of the data for both the soft muting of the sample rate converter and the scaling of the input data by the sample rate ratio before storing the samples in the RAM. The input data is scaled by the sample rate ratio because as the FIR filter length of the convolution increases, so does the amplitude of the convolution output. To keep the output of the FIR filter from saturating, the input data is scaled down by multiplying it by $\mathrm{f}_{\mathrm{S}_{\text {_OUT }}} / \mathrm{f}_{\mathrm{S}_{\text {_ }}} \mathrm{IN}$
 muting and unmuting the AD1895.
The RAM in the FIFO is 512 words deep for both left and right channels. A small offset of 16 is added to the write address provided by the $\mathrm{f}_{\mathrm{S}_{-} \mathrm{IN}}$ counter to prevent the RAM read pointer from ever overlapping the write address. The maximum decimation rate can be calculated from the RAM word depth as $(512-16) / 64$ taps $=7.75$ and a small offset.


Figure 8. Frequency Response of the Digital Servo Loop. $f_{S_{-} I N}$ is the $x$-axis, $f_{S_{-} \text {out }}=192 \mathrm{kHz}$, master clock frequency is 30 MHz .

The digital servo loop is essentially a ramp filter that provides the initial pointer to the address in RAM and ROM for the start of the FIR convolution. The RAM pointer is the integer output of the ramp filter, while the ROM is the fractional part. The digital servo loop must be able to provide excellent rejection of jitter on the $f_{S_{\text {_IN }}}$ and $f_{S_{\text {_ out }}}$ clocks as well as measure the arrival of the $\mathrm{f}_{\text {S_OUT }}$ clock within 4.97 ps. The digital servo loop will also divide the fractional part of the ramp output by the ratio of $\mathrm{f}_{\mathrm{S}_{\text {IN }}} / \mathrm{f}_{\mathrm{S}_{-} \text {out }}$ for the case when $\mathrm{f}_{\text {S_IN }}>\mathrm{f}_{\mathrm{S}_{-} \text {out }}$, to dynamically alter the ROM coefficients.
The digital servo loop is implemented with a multirate filter. To settle the digital servo loop filter quicker upon startup or a change in the sample rate, a Fast Mode was added to the filter. When the digital servo loop starts up or the sample rate is changed, the digital servo loop kicks into Fast Mode to adjust and settle on the new sample rate. Upon sensing the digital servo loop settling down to some reasonable value, the digital servo loop will kick into Normal or Slow Mode. During Fast Mode, the MUTE_OUT signal of the sample rate converter is asserted to let the user know that they should mute the sample rate converter to avoid any clicks or pops. The frequency response of the digital servo loop for Fast Mode and Slow Mode are shown in Figure 8.

The FIR filter is a 64 -tap filter in the case of $\mathrm{f}_{\mathrm{S}_{-} \text {out }} \geq \mathrm{f}_{\mathrm{S}_{-} \mathbb{N}}$ and is $\left(\mathrm{f}_{\mathrm{S}_{-} \mathrm{IN}} / \mathrm{f}_{\mathrm{S}_{\text {_OUT }}}\right) \times 64$ taps for the case when $\mathrm{f}_{\mathrm{S}_{-} \mathrm{IN}}>\mathrm{f}_{\mathrm{S}_{-} \text {out. }}$. The FIR filter performs its convolution by loading in the starting address of the RAM address pointer and the ROM address pointer from the digital servo loop at the start of the $\mathrm{f}_{\mathrm{S} \text { _out }}$ period. The FIR filter then steps through the RAM by decrementing its address by 1 for each tap, and the ROM pointer increments its address by the $\left(\mathrm{f}_{\mathrm{S}_{\text {_OUT }}} / \mathrm{f}_{\mathrm{S}_{-} \mathrm{IN}}\right) \times 2^{20}$ ratio for $\mathrm{f}_{\mathrm{S}_{\text {IN }}}>\mathrm{f}_{\mathrm{S}_{\text {_out }}}$ or $2^{20}$ for $\mathrm{f}_{\mathrm{S}_{-} \text {out }} \geq \mathrm{f}_{\mathrm{S}_{\text {_IN }}}$. Once the ROM address rolls over, the convolution is completed. The convolution is performed for both the left and right channels, and the multiply accumulate circuit used for the convolution is shared between the channels.

The $\mathrm{f}_{\text {S_IN }} / \mathrm{f}_{\text {S_out }}$ sample rate ratio circuit is used to dynamically alter the coefficients in the ROM for the case when $f_{S_{-}}>f_{S_{\text {_OUT }}}$. The ratio is calculated by comparing the output of an $\mathrm{f}_{\mathrm{S}_{\mathrm{L}} \text { out }}$ counter to the output of an $f_{S_{S} I N}$ counter. If $f_{S_{-} O U T}>f_{S_{-} I N}$, the ratio is held at 1 . If $f_{S_{-I N}}>f_{S_{-} \text {out }}$, the sample rate ratio is updated if it is different by more than two $\mathrm{f}_{\mathrm{S}_{\mathrm{S}}}$ out periods from the previous $f_{S_{\text {_OUT }}}$ to $f_{S_{\text {_IN }}}$ comparison. This is done to provide some hysteresis to prevent the filter length from oscillating and causing distortion.

## OPERATING FEATURES

## RESET and Power-Down

When RESET is asserted low, the AD1895 will turn off the master clock input to the AD1895, MCLK_IN, initialize all of its internal registers to their default values, and three-state all of the I/O pins. While RESET is active low, the AD1895 is consuming minimum power. For the lowest possible power consumption while $\overline{\text { RESET }}$ is active low, all of the input pins to the AD1895 should be static.
When $\overline{\text { RESET }}$ is deasserted, the AD1895 begins its initialization routine where all locations in the FIFO are initialized to zero, MUTE_OUT is asserted high, and any I/O pins configured as outputs are enabled. The mute control counter, which controls the soft mute attenuation of the input samples, is initialized to maximum attenuation, -127 dB (see Mute Control section).
When asserting $\overline{\text { RESET }}$ and deasserting $\overline{\text { RESET, }}$, the $\overline{\text { RESET }}$ should be held low for a minimum of five MCLK_IN cycles. During power-up, the $\overline{\text { RESET }}$ should be held low until the power supplies have stabilized. It is recommended that the AD1895 be reset when changing modes.

## Power Supply and Voltage Reference

The AD1895 is designed for 3 V operation with 5 V input tolerance on the input pins. VDD_CORE is the 3 V supply that is used to power the core logic of the AD1895 and to drive the output pins. VDD_IO is used to set the input voltage tolerance of the input pins. In order for the input pins to be 5 V input tolerant, VDD_IO must be connected to a 5 V supply. If the input pins do not have to be 5 V input tolerant, then VDD_IO can be connected to VDD_CORE. VDD_IO should never be less than VDD_CORE. VDD_CORE and VDD_IO should be bypassed with 100 nF ceramic chip capacitors as close to the pins as possible to minimize power supply and ground bounce caused by inductance in the traces. A bulk aluminium electrolytic capacitor of $47 \mu \mathrm{~F}$ should also be provided on the same PC board as the AD1895.

## Digital Filter Group Delay

The filter group delay is given by the equation:

$$
\begin{aligned}
& G D=\frac{16}{f_{S_{-} I N}}+\frac{32}{f_{S_{-} I N}} \text { seconds for } f_{S_{-} \text {OUT }}>f_{S_{-} I N} \\
& G D=\frac{16}{f_{S_{-} I N}}+\left(\frac{32}{f_{S_{-} I N}}\right) \times\left(\frac{f_{S_{-} I N}}{f_{S_{-} O U T}}\right) \text { seconds for } f_{S_{-} \text {OUT }}<f_{S_{-} I N}
\end{aligned}
$$

## Mute Control

When the MUTE_IN pin is asserted high, the MUTE_IN control will perform a soft mute by linearly decreasing the input data to the AD1895 FIFO to almost zero, -127 dB attenuation. When MUTE_IN is deasserted low, the MUTE_IN control will linearly decrease the attenuation of the input data to 0 dB . A 12-bit counter, clocked by LRCLK_I, is used to control the mute attenuation. Therefore, the time it will take from the assertion of MUTE_IN to -127 dB full mute attenuation is 4096/LRCLK_I seconds. Likewise, the time it will take to reach 0 dB mute attenuation from the deassertion of MUTE_IN is 4096/LRCLK_I seconds.

Upon RESET, or a change in the sample rate between LRCLK_I and LRCLK_O, the MUTE_OUT pin will be asserted high. The MUTE_OUT pin will remain asserted high until the digital servo loop's internal Fast Settling Mode has completed. When the digital servo loop has switched to Slow Settling Mode, the MUTE_OUT pin will deassert. While MUTE_OUT is asserted, the MUTE_IN pin should be asserted as well to prevent any major distortion in the audio output samples.

## Master Clock

A digital clock connected to the MCLK_IN pin or a fundamental or third overtone crystal connected between MCLK_IN and MCLK_OUT can be used to generate the master clock, MCLK_IN. The MCLK_IN pin can be 5 V input tolerant just like any of the other AD1895 input pins. A fundamental mode crystal can be inserted between MCLK_IN and MCLK_OUT for master clock frequency generation up to 27 MHz . For master clock frequency generation with a crystal beyond 27 MHz , it is recommended that the user use a third overtone crystal and add an LC filter at the output of MCLK_OUT to filter out the fundamental, do not notch filter the fundamental. Please refer to your quartz crystal supplier for values for external capacitors and inductor components.


Figure 9a. Fundamental Mode Circuit Configuration


Figure 9b. Third Overtone Circuit Configuration
There are, of course, maximum and minimum operating frequencies for the AD1895 master clock. The maximum master clock frequency at which the AD 1895 is guaranteed to operate is 30 MHz .30 MHz is more than sufficient to sample rate convert sampling frequencies of $192 \mathrm{kHz}+12 \%$. The minimum required frequency for the master clock generation for the AD1895 depends upon the input and output sample rates. The master clock has to be at least 138 times greater than the maximum input or output sample rate.

## AD1895

## Serial Data Ports—Data Format

The Serial Data Input Port Mode is set by the logic levels on the SMODE_IN_0/SMODE_IN_1/SMODE_IN_2 pins. The serial data input port modes available are left justified, $\mathrm{I}^{2} \mathrm{~S}$, and right justified (RJ), 16, 18, 20, or 24 bits, as defined in Table I.

Table I. Serial Data Input Port Mode

| SMODE_IN_[0:2] |  |  |  |
| :--- | :---: | :--- | :--- |
| $\mathbf{2}$ | $\mathbf{1}$ | $\mathbf{0}$ |  |
| 0 | 0 | 0 | Left Justified |
| 0 | 0 | 1 | $\mathrm{I}^{2}$ S |
| 0 | 1 | 0 | Undefined |
| 0 | 1 | 1 | Undefined |
| 1 | 0 | 0 | Right Justified, 16 Bits |
| 1 | 0 | 1 | Right Justified, 18 Bits |
| 1 | 1 | 0 | Right Justified, 20 Bits |
| 1 | 1 | 1 | Right Justified, 24 Bits |

The Serial Data Output Port Mode is set by the logic levels on the SMODE_OUT_0/SMODE_OUT_1 and WLNGTH_OUT_0/ WLNGTH_OUT_1 pins. The serial mode can be changed to left justified, $\mathrm{I}^{2} \mathrm{~S}$, right justified, or TDM as defined in the Table II. The output word width can be set by using the WLNGTH_OUT_0/ WLNGTH_OUT_1 pins as shown in

Table III. When the output word width is less than 24 bits, dither is added to the truncated bits. The Right-Justified Serial Data Out Mode assumes 64 SCLK_O cycles per frame, divided evenly for left and right. The AD1895 also supports 16-bit, 32-clock packed input and output serial data in LJ, RJ, and I ${ }^{2}$ S format.

Table II. Serial Data Output Port Mode

| SMODE_OUT_[0:2] |  | Interface Format |
| :--- | :---: | :--- |
| $\mathbf{1}$ | $\mathbf{0}$ |  |
| 0 | 0 | Left Justified (LJ) |
| 0 | 1 | IS |
| 1 | 0 | TDM Mode |
| 1 | 1 | Right Justified (RJ) |

Table III. Word Width

| WLNGTH_OUT_[0:1] |  | Word Width |
| :--- | :---: | :--- |
| $\mathbf{1}$ | $\mathbf{0}$ |  |
| 0 | 0 | 24 Bits |
| 0 | 1 | 20 Bits |
| 1 | 0 | 18 Bits |
| $\mathbf{1}$ | 1 | 16 Bits |

The following timing diagrams show the serial mode formats.


Figure 10. Input/Output Serial Data Formats

## TDM MODE APPLICATION

In TDM Mode, several AD1895s can be daisy-chained together and connected to the serial input port of a SHARC ${ }^{\circledR}$ DSP. The AD1895 contains a 64 -bit parallel load shift register. When the LRCLK_O pulse arrives, each AD1895 parallel loads its left and right data into the 64 -bit shift register. The input to the shift register is connected to TDM_IN, while the output is connected to SDATA_O. By connecting the SDATA_O to the TDM_IN
of the next AD1895, a large shift register is created and is clocked by SCLK_O.
The number of AD1895s that can be daisy-chained together is limited by the maximum frequency of SCLK_O, which is about 25 MHz . For example, if the output sample rate, $\mathrm{f}_{\mathrm{S}}$, is 48 kHz , up to eight AD1895s could be connected since $512 \times \mathrm{f}_{\mathrm{S}}$ is less than 25 MHz . In Master/TDM Mode, the number of AD1895s that can be daisy-chained is fixed to four.


Figure 11. Daisy-Chain Configuration for TDM Mode (All AD1895s Being Clock-Slaves)


Figure 12. Daisy-Chain Configuration for TDM Mode (First AD1895 Being Clock-Master)

## Serial Data Port Master Clock Modes

Either of the AD1895 serial ports can be configured as a master serial data port. However, only one serial port can be a master, while the other has to be a slave. In Master Mode, the AD1895 requires a $256 \times \mathrm{f}_{\mathrm{S}}, 512 \mathrm{f}_{\mathrm{S}}$, or $768 \times \mathrm{f}_{\mathrm{S}}$ master clock (MCLK_IN). For a maximum master clock frequency of 30 MHz , the maximum sample rate is limited to 96 kHz . In Slave Mode, sample rates up to 192 kHz can be handled.
When either of the serial ports is operated in Master Mode, the master clock is divided down to derive the associated left/right subframe clock (LRCLK) and serial bit clock (SCLK). The master clock frequency can be selected for 256,512 , or 768 times the input or output sample rate. Both the input and output serial ports will support Master Mode LRCLK and SCLK generation for all serial modes, left justified, $I^{2}$ S, right justified, and TDM for the output serial port.

Table IV. Serial Data Port Clock Modes

| MMODE_0/ MMODE_1/ MMODE_2 |  |  | Interface Format |
| :---: | :---: | :---: | :---: |
| 2 | 1 | 0 |  |
| 0 | 0 | 0 | Both Serial Ports Are in Slave Mode |
| 0 | 0 | 1 | Output Serial Port Is Master with $768 \times \mathrm{f}_{\text {S_OUT }}$ |
| 0 | 1 | 0 | Output Serial Port Is Master with $512 \times \mathrm{f}_{\text {S_out }}$ |
| 0 | 1 | 1 | Output Serial Port Is Master with $256 \times \mathrm{f}_{\text {S_out }}$ |
| 1 | 0 | 0 | Undefined |
| 1 | 0 | 1 | Input Serial Port Is Master with $768 \times \mathrm{f}_{\text {S_IN }}$ |
| 1 | 1 | 0 | Input Serial Port Is Master with $512 \times \mathrm{f}_{\text {S_IN }}$ |
| 1 | 1 | 1 | Input Serial Port Is Master with $256 \times \mathrm{f}_{\text {S_IN }}$ |

## Bypass Mode

When the BYPASS pin is asserted high, the input data bypasses the sample rate converter and is sent directly to the serial output port. Dithering of the output data when the word length is set to less than 24 bits is disabled. This mode is ideal when the input and output sample rates are the same and LRCLK_I and LRCLK_O are synchronous with respect to each other. This mode can also be used for passing through nonaudio data, since no processing is performed on the input data in this mode.

## OUTLINE DIMENSIONS

## 28-Lead Shrink Small Outline Package [SSOP] (RS-28)

Dimensions shown in millimeters

Location Page9/02-Data Sheet changed from REV. A to REV. B.
Changes to SPECIFICATIONS (Digital Performance) .....  2
Changes to SPECIFICATIONS (Digital Timing) ..... 3
Changes to ORDERING GUIDE ..... 5
Replaced TPCs 1-52 .....  7
Additions to $\overline{\mathrm{RESET}}$ and Power-Down section ..... 19
Changes to Figures 9a and 9b ..... 19
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Updated OUTLINE DIMENSIONS ..... 23


[^0]:    *Patents pending.

[^1]:    NOTES
    ${ }^{1}$ Lower sampling rates than those given by this formula are possible, but the jitter rejection will decrease.
    ${ }^{2}$ Refer to the Typical Performance Characteristics section for DNR and THD + N numbers over a wide range of input and output sample rates.
    ${ }^{3}$ For any other ratio, minimum THD +N will be better than -115 dB . Please refer to detailed performance plots.
    Specifications subject to change without notice.

